

**A MAXWELL THEORY FOR THE SCATTERING OF TM POLARIZED  
ELECTROMAGNETIC BEAMS  
BY A DOUBLE METALLIC SLIT**

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**Resumen.**

Se presenta una teoría vectorial de la difracción de haces Hermite–Gauss sobre una pantalla metálica de espesor  $h$  con dos rendijas de ancho  $\ell$  y separación  $d$ . los haces inciden oblicuamente con polarización TM. Estudiamos numéricamente los patrones de difracción en campo lejano como función de los parámetros opto–geométricos: longitud de onda  $\lambda$ , ancho de rendija  $\ell$ , separación  $d$ , ángulo de incidencia  $\theta_i$  y orden del polinomio de Hermite  $m$ . Por otra parte, en la región vectorial de la difracción dada por  $\lambda/\ell > 0.2$  donde  $\lambda$  es la longitud de onda incidente, se analiza numéricamente la energía difractada a lo largo de la dirección del haz incidente ( $E_i$ ) y la validez de la propiedad de la difracción escalar  $E_i = N\tau/\lambda$  donde  $\tau$  es el coeficiente de transmisión y  $N$  el número de rendijas.

**Abstract**

We present a rigorous theory for oblique incident Hermite-Gaussian beams, diffracted by two slits of width  $\ell$  and separation  $d$ , in a thick metallic screen for the case of polarization TM(S). The far field spectra as a function of several opto-geometrical parameters, wavelength  $\lambda$ , slit width  $\ell$ , separation  $d$ , incidence angle  $\theta_i$  and Hermite order  $m$  is analyzed. In the vectorial diffraction region given when  $\lambda/\ell > 0.2$ , where  $\ell$  is the incident wavelength and as a function of the separation between slits  $d$ ; we have numerically analyzed: the far field spectra, the energy diffracted along the incident beam direction ( $E_i$ ), and the validity of an approximate diffraction (scalar) property, namely  $E_i = N\tau/\lambda$ .

**Palabras clave:**

Difracción, Esparcimiento, Doble rendija.

**Keywords:**

Diffraction, Scattering, Double slit.

## **Introduction.**

Currently there are several rigorous theories of diffraction by plane electromagnetic waves (Enriquez *et al.*, 2011) and Gaussian beams (Mata *et al.*, 1993); (Mata *et al.*, 1994) by two slits in metallic screens of zero thickness. However these theories do not treat with Hermite-Gauss or oblique incidence, nor thick screens of nonzero thickness (Mata *et al.*, 2008).

In this paper, we present a novel rigorous theory of diffraction that allows to consider the illumination by Hermite-Gaussian beams at oblique incidence on two slits of width  $\ell$  and separation  $d$  in screens with infinite conductivity and thickness  $h$ .

We analyze the coupling between slits through the numerical study of the diffracted energy along the direction of the incident ( $E_i$ ) beam energy as a function of the parameter of separation  $d$  between the slits. It is revealed the existence of oscillations in the energy  $E_i$ . We also show that in the case of TM(S) polarization, the energy  $E_i$  is special because when compared to other diffraction patterns. Finally, we show that the scalar property valid at the scalar region ( $\lambda/\ell < 0.2$ )  $E_i = N\tau/\lambda$  (Alvarez-Cabanillas, 1995) is no longer valid.

## **A Vector Theory of Diffraction.**

In Fig.1 we have two slits on a screen of infinite conductivity, and non-zero thickness denoted by  $h$ . In this screen, you have two parallel to the Oz axis,  $\ell$  wide and spaced slits  $d$ . The display is in the gap and impinges perpendicularly on it a Hermite-Gaussian beam with wavelength  $\lambda = 2\pi/k$  and order  $m$ . We will use the complex representation for the fields and omit the time factor going forward  $e^{-i\omega t}$ .  $H$  is the magnetic field when you have the TM (magnetic field parallel to the axis Oz) polarization. The  $H$  field satisfies the Helmholtz equation (Mata *et al.*, 1994).

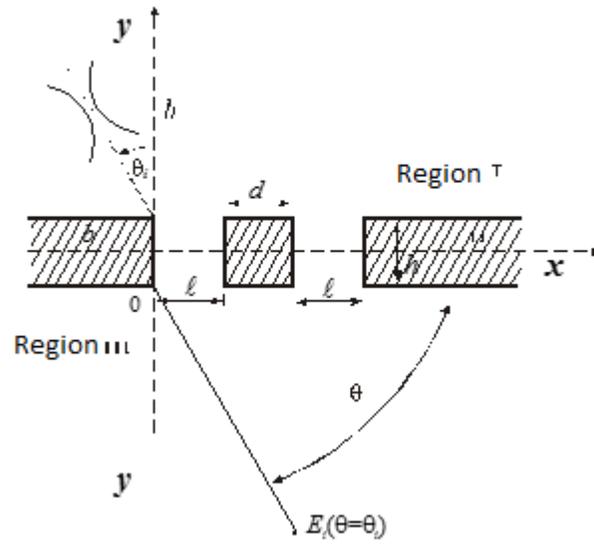
$$\partial^2 H / \partial x^2 + \partial^2 H / \partial y^2 + k^2 H = 0. \quad (1)$$

Denote by  $H_I$  the solution of Eq (1) in the region I ( $y > h/2$ ), expressed by a plane wave expansion:

$$H_I(x, y) = \frac{1}{\sqrt{2\pi}} \int_{-k}^k A(\alpha) e^{i(\alpha x - \beta y)} d\alpha + \frac{1}{\sqrt{2\pi}} \int_{-k}^k B(\alpha) e^{i(\alpha x + \beta y)} d\alpha \quad (2)$$

The first integral is identified with the incident beam due to the sign of the  $\alpha$  and  $\beta$  k-components.

In region II, within the screen,  $-h/2 < y < h/2$  the electromagnetic field will be represented by the following modal series:



**Figure 1.** Our system. Two slits of width  $\ell$  and spacing  $d$  in an infinitely thick conducting screen  $h$ . The energy diffracted along the incident direction ( $E_i$ ) is diffracted in the direction of  $\theta$  (relative to the axis  $Oy$ ) =  $\theta_i$  (From the axis  $Ox$ ).

$$H_{II}(x, y) = \sum_{n=0}^{\infty} a_n^1 \varphi_n^1(x, y) + \sum_{n=0}^{\infty} a_n^2 \varphi_n^2(x, y) \quad (3)$$

Where in  $i = 1, 2$  the set  $\varphi_n^i(x)$ , are functions whose normal derivative is zero at the walls for the TM polarization.

The diffracted field below the screen, for  $y < -h/2$  (region III), could be expressed as a plane wave expansion too:

$$H_{III}(x, y) = \frac{1}{\sqrt{2\pi}} \int_{-\infty}^{\infty} C(\alpha) e^{i(\alpha x + \beta y)} d\alpha \quad (4)$$

Our goal is to determine the transmitted field (Eq. (4)), for which one needs to determine  $C(\alpha)$ . Note that  $C(\alpha)$  depends on the coefficients  $a_n^1$  and  $a_n^2$  and the incident amplitude  $A(\alpha)$ . For this, we use the appropriate conditions of continuity, which could be obtained from Maxwell's equations (Alvarez-Cabanillas, 1995). These conditions lead us to the following matrix system, in which the matrix columns  $\mathbf{a}_1$  and  $\mathbf{a}_2$  are formed respectively by the coefficient  $a_n^1$  and  $a_n^2$ .

$$\mathbf{M}_{11}\mathbf{a}_1 + \mathbf{M}_{12}\mathbf{a}_2 = \mathbf{S}_1, \quad (5)$$

$$\mathbf{M}_{21}\mathbf{a}_1 + \mathbf{M}_{22}\mathbf{a}_2 = \mathbf{S}_2,$$

where  $M_{ik}$  ( $i, k = 1, 2$ ) are square matrices dependent on the opto-geometrical parameters and  $S_i$  ( $i = 1, 2$ ) are matrices depending only on  $A(\alpha)$ . The determination of the modal coefficients  $a_n^1$  and  $a_n^2$  allow us to calculate the diffracted field in any region for TM polarization.

## Results and Discussion.

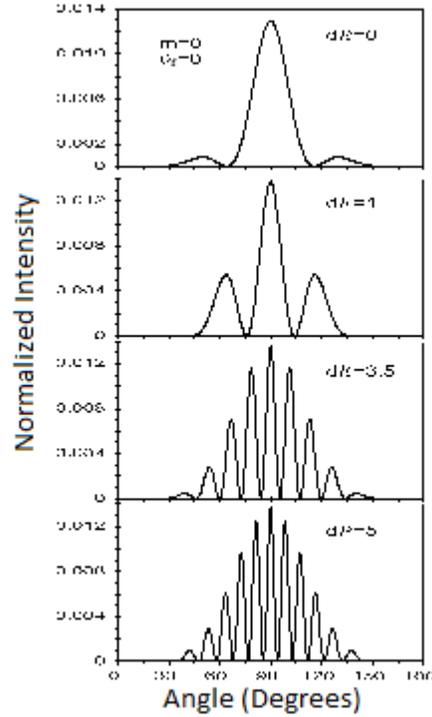
Using the complex Poynting vector is possible to obtain the diffracted intensity at the angle  $\theta$ . For a Hermite-Gaussian beam, the spectral amplitude is (Mata *et al*, 2008):

$$A(\alpha) = \frac{L}{2} i^m H_m \left[ -\frac{L}{2} (\alpha \sin \theta_i - \beta \cos \theta_i) \right] \times \left[ \sin \theta_i + \left( \frac{\alpha}{\beta} \right) \cos \theta_i \right] e^{(-i\alpha b)} \times e^{[-(\alpha \sin \theta_i - \beta \cos \theta_i)^2 L^2 / 8]} \quad (6)$$

where  $H_m$  is the Hermite polynomial of order  $m$ . The position of the beam waist is given by the parameter  $b$  (see Fig. 1).

In the figures relating to energy diffracted along the direction of the incident beam is  $E_i(\theta = \theta_i)$  the diffracted angle in the direction of the incident beam, measured from the axis Ox and  $\theta_i$  is the angle of incident beams to the axis Oy measured. The energy, the diffracted intensity  $I(\theta)$  and the transmission coefficient  $\tau$  are normalized to the total incident energy  $I_0$ . All parameters normalized opto-geometrical width of the slots  $\ell$ , that is,  $\ell = 1$ .

In Figs. 2 and 3 show the diffraction patterns of Hermite-Gaussian beams for the fundamental mode  $m = 0$  at normal incidence and oblique incidence of  $30^\circ$ ; the wavelength of the incident beams is  $\lambda/\ell=0.9$ , with extremely wide Gaussian beams  $L/\ell= 500/\sqrt{2}$  and fixed at the position  $b/\ell=0.5$ , the thickness of the screen is  $h/\ell = 1$  and the gaps between slits are  $d/\ell= 0, 1, 3.5$  and  $5$ .

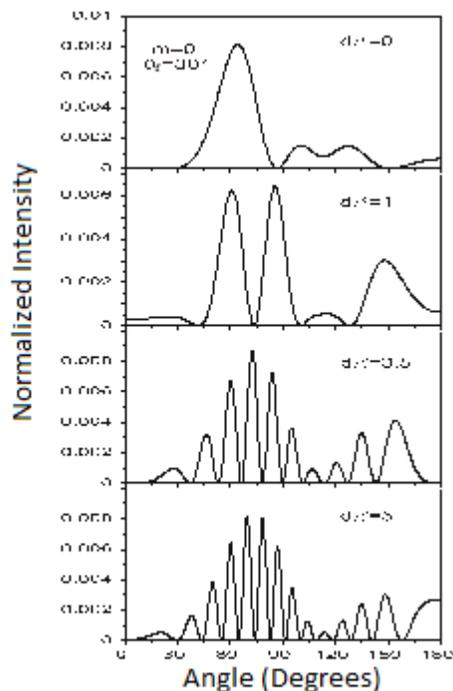


**Figure 2.** Diffraction patterns normalized  $(I(\theta)/I_0)$  of Hermite-Gaussian beams of  $m = 0$  normally incident on two slits so. With  $\lambda/\ell = 0.9$ ,  $L/\ell=500/\sqrt{2}$ ,  $h/\ell = 1$  and position  $b/\ell=0.5$  and for separations  $d/\ell = 0, 1, 3.5$  and  $5$ .

The shape of the diffraction patterns for the  $m = 2$  mode, not shown, is identical to the spectra of FIGS. 2 and 3 (with the same opto-geometrical parameters) except for a scaling factor which provides a lower intensity for this mode, from the respective Hermite polynomial.

From these diffraction patterns, we have taken the diffracted energy  $E_i$  along the direction of the incident beams. Figs. 4 and 5 show the behavior of the  $E_i$  separation according to  $d$  for  $m = 0$  and  $2$  modes; opto-geometrical parameters of these figures are the same in Fig. 2 and 3.

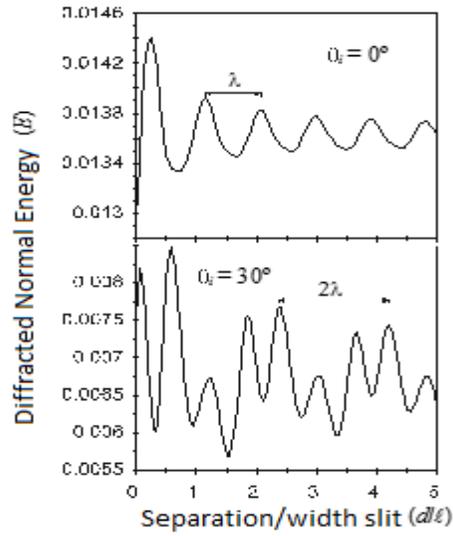
The curves of FIGS. 4 and 5 show the oscillatory behaviors as  $E_i$  a function of the spacing  $d$ , for the period is normal incidence to oblique incidence  $\lambda$  and the period is  $2\lambda$ .



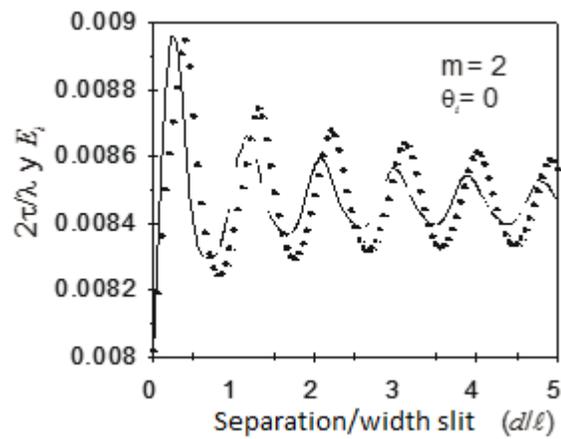
**Figure 3.** Standard diffraction patterns ( $I(\theta)/I_0$ ) Hermite-Gaussian beam for  $m = 0$  to  $30^\circ$  obliquely incident on two slits so. Same parameters of Fig.2.

In Fig. 5 has also been drawn in broken lines the  $2\tau/\lambda$  function. As you can see, this function does not overlap with the energy with  $E_i$  which we can say that the property of diffraction  $E_i = 2\tau/\lambda$  is not valid in the vector region at least for the separation parameter  $d$  and doing extremely wide.

Finally, in Fig. 6 different diffracted energy around the energy is  $E_i$ . The upper curves of Figure 6 correspond to normal incidence for the  $m = 2$  mode, with the same parameters of Fig. 3; diffracted energies correspond to the angles diffracted  $\theta = 90^\circ, 91^\circ, 92^\circ$  and  $94^\circ$ . The curves in the lower window of Fig. 6 correspond to oblique incidence of  $30^\circ$ , also for mode  $m = 2$ , with the same parameters of Fig. 4. The diffracted energies shown, corresponding to angles diffracted around of  $\theta = 60^\circ$  (corresponding to the diffracted energy along the oblique incidence angle  $\theta_i = 30^\circ$ ) and for the angles  $58^\circ, 57^\circ$  and  $64^\circ$ .

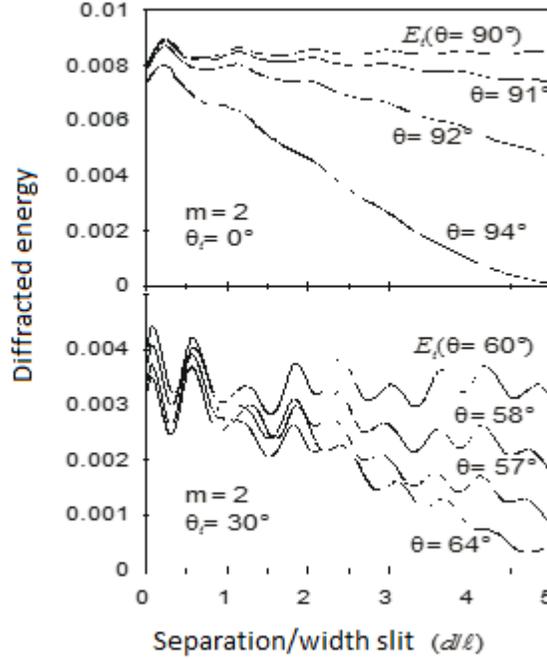


**Figure 4.** Energy diffracted in the direction normal to the standard  $E_i$  to Hermite-Gauss beam, depending on the spacing  $d/l$  screen. For the fundamental mode  $m = 0$ , at normal incidence and oblique incidence of  $30^\circ$ , with  $\lambda/l=0.9$ ,  $L/l=500/\sqrt{2}$ ,  $h/l=1$ ,  $y b/l=0.5$ .



**Figure 5.** Energy diffracted in the direction normal to the  $E_i$  (solid line) Hermite-Gauss beam, thus  $m = 2$  and  $2\tau/\lambda$  property (dashed line), in function of the spacing  $d/l$ . Same parameters of Fig. 3.

Energy analyzing energy diffracted  $E_i$  around for  $m = 0$  at normal incidence and oblique incidence of  $30^\circ$  as also carried out (data not shown) found similar patterns for mode  $m = 2$  (see Fig. 6), the energy diffracted around the energy as  $E_i$  a function of the spacing  $d$ , decay to zero.



**Figure 6.** Energy diffracted around energy  $E_i(\theta = \theta_i)$  Hermite-Gauss beam, for the  $m = 2$  mode according to the distance between slits  $d/\ell$ . Same parameters of Fig. 4.

### Conclusion.

Present a more rigorous theory of diffraction for the oblique incidence beam Hermite-Gaussian (HG) on a screen of thickness  $h$  with wide slits separating slits  $\ell$  and  $d$ . In the case of TM(S) polarization and wavelengths in the vector region  $\frac{\lambda}{\ell} > 0.2$ , we have found that the diffracted along the direction of the incident beam energy has oscillations period  $\lambda$  as a function of the spacing  $d$  for modes  $m = 0$  and  $2$ , for the period  $2\lambda$  at  $30^\circ$  oblique incidence. Finally, we note that the energy  $E_i$  has special characteristics compared diffracted energies in other directions and found numerically that ownership of scalar diffraction ( $\lambda/\ell < 0.2$ ) given by  $E_i = 2\tau/\lambda$  is no longer valid in this region ( $\lambda/\ell > 0.2$ ).

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